Application: AEF-A.1 Cantilever beam

KEY WORDS

Static linear analysis, Planar geometric model, Plane stress state, Linear material, Planar 2D finite element, Linear finite element, Machine element, Checking with classical models, Cantilever beam

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A. PROBLEM DESCRIPTION

A.1 Introduction

In many training situations to solve AEF problems, especially as a beginner or initiating a new AEF platform, it is recommended to solve simple problems that are reduced to classic models with known analytical solutions.

The primary objective of this application involves developing an AEF for a rectangular beam bar structure and comparing the results with the classical analytical ones.

A.2 Application description

In the structure of the support device below, the elastic support member 1, firmly positioned in the body 2 by the rods 4 and the screws 5, must provide a displacement imposed by the push force F developed by the skate 3 and return to the state initially after its cancellation.



For this application, it is necessary to analyse the displacement, deformation and tension fields of the bearing element 1 made of C55 steel and having the following dimensions: L = 100, h = 10 mm, g = 10 mm, a = 50 mm, b = 20 mm. After analysing the structure from the fact that the element 1 has a constant thickness and

the force loading, F = 1000 N, it produces evenly the width, it is highlighted the framing of the problem in the flat tension state (the tensions are invariant to thickness).

B. THE FEA MODEL

B.1 The model definition

In order to compare the results obtained by the finite element analysis with the classical solution model based on the material resistance methods (embedded beam), the most simplified possible model is adopted which implies:

- simple geometric shape,
- adoption of material strengthens constraints (embedding)
- the loads are concentrated,
- the material has a linear behavior

B.2 The analysis model description

Because the structure is framed in the AEF plane stress state, it can be modelled in plane, considering the rectangular geometric shape 100 mm long and 10 mm wide with 2D finite elements.

Geometric constraints involving cancellations of translation and rotation relative to the X, Y and Z axes, respectively, apply to the points on the Y-axis edge. Load the model with the concentrated force F = 1000 N in the far upper corner.



• longitudinal modulus of elasticity, $E = 210000 \text{ N} / \text{mm}^2$;

• Poisson's ratio, v = 0,3.

Average working temperature of the subassembly, $T_0 = 20 \circ C$.

C. PREPROCESSING OF FEA MODEL



C.2 Modelling of material and environment characteristics
\land \rightarrow Project Schematic \rightarrow \downarrow \checkmark Engineering Data \checkmark \checkmark \rightarrow \downarrow \checkmark Edit \rightarrow Outline of Schematic A2: Engineering Data \cdot \downarrow
🗞 Structural Steel , Properties of Outline Row 3: Structural Steel 😑 🎦 Isotropic Elasticity 🛶 Young's Modulus , [selecting from
drop down list, C (Unit) with $\downarrow \checkmark$, $\downarrow MPa$], [enter in column, B (Unit) valoarea / value, 210000] $\rightarrow \downarrow$
\checkmark Update Project $\rightarrow \downarrow \bigcirc$ Return to Project (others parameters are default).

C 3 Geometric modelling
C 2.1 Me delle a dine. Device Me deler (DM)
C.3.1 Model loading, DesignModeller (DM)
C.3.2 Sketch generation
Viewing default plane (XY)
$\textcircled{W} \rightarrow \square$ Sketching $\rightarrow \swarrow$ (Look At Face/Plane/Sketch) [automatically view of default plane, XY].
<u>Rectangular line generation</u>
\downarrow Draw \rightarrow \downarrow Rectangle \rightarrow [trace rectangle line using pencil starting with, \downarrow , from coordinates system origin
(appear symbol, P), and finish in opposite point simultaneously with release of the mouse fig. a)]
<u>Dimensions</u>
\downarrow Dimensions $\rightarrow \downarrow^{\texttt{Semi-Automatic}} \rightarrow [automatically create dimensions with \downarrow] \rightarrow \downarrow^{\texttt{Details View}},$
Dimensions: 2: U1, [enter value, 10]; U2, [enter value, 100] (fig. b). UB Display (view dimensions),
Name: , [activate), Value: , IV (activate). , Move (move dimensions), [activate dimension with, , and
move kipping active until in target position] (fig. b).
p p p p p p p p p p p p p p p p p p p
10,000
<i>a. b.</i>
C.3.3 Surface generation
$\bigcirc \rightarrow \Box_{\text{Concept}} \rightarrow \Box_{\text{Surfaces From Sketches}} \rightarrow Details View,$
$\Box \text{ Details of SurfaceSk1} \qquad Base Objects \qquad \rightarrow \qquad \Box \oplus \checkmark \checkmark XYPlane,$
$\downarrow \checkmark \checkmark \checkmark \checkmark \land $
\rightarrow \downarrow $\stackrel{\neq}{\rightarrow}$ Generate \sqsubseteq \checkmark \checkmark Sketch1 \rightarrow \downarrow \bigcirc Hide Sketch (hide sketch), \downarrow
(inde bioten).
Lither way in the second seco
Details of Surface Body Body [enter name, Suprafată bară]
C.3.4 Save of geometric model
$\textcircled{0} \rightarrow \Box [(Save Project) \rightarrow \Box (Close).$



Outline 🛶 🗇 🕀 Geometry 🛶 🗸 🐨 🖓 Suprafață bară 🚽 Details of "Suprafață bară": Material : Assignment , [selecting]
from the list \downarrow \downarrow Structural Steel usually, when there is only one item, this setting is default).
Setting the units
🕅 🛶 Units 🛶 Metric (mm, kg, N, s, mV, mA)



D. SOLVING THE AEF MODEL

D.1. Selecting the results types
$\textcircled{Outline} \rightarrow \square$ $\textcircled{Outline}$ \bigcirc \square $\textcircled{Outline}$ \bigcirc \bigcirc \bigcirc \bigcirc \bigcirc $\textcircled{Outline}$ \bigcirc
$ = \frac{1}{2} \xrightarrow{1} \sqrt{2} $ Solution (A6) $\rightarrow 1$ $\sqrt{2}$ Stress $\rightarrow 1$ $\sqrt{2}$ Normal $\rightarrow 2$ Details of "Normal Stress", $= 2$ Definition Orientation,
[selecting from drop down list ,]X Axis] (default selection).



E. POST-PROCESSING OF RESULTS





F. RESULTS ANALYSIS

F.1 Theoretical (analytical) calculus model

Classical analytical studies on the analysed structure (embedded bar) can be synthesized in the calculation of the parameters:

- maximum displacement,

$$\delta = \frac{\mathrm{Fl}^3}{3 \mathrm{EL}_2} = \frac{4 \mathrm{Fl}^3}{\mathrm{E \ b \ h^3}} = \frac{4 \mathrm{10}^3 \mathrm{10}^6}{2 \mathrm{10}^5 \mathrm{10} \mathrm{10}^3} = 2 \mathrm{mm};$$

- the maximum bending stress (Navier's relationship),

$$\sigma_i = \frac{M_i}{W_z} = \frac{6 F l}{b h^2} = \frac{610^3 10^2}{1010^2} = 600 \text{ MPa};$$

- maximum tangential shear stress (Juravschi's relationship),



Taking into consideration the results obtained using the modelling and AEF (sub-chapter E) and the use of the classical calculus relations (subchapters E and F.1) obtained under the conditions of the strengthens of the materials, the following are highlighted:

- the maximum displacement of 2,0142 mm obtained with AEF (E.1) is the same with the displacement (2 mm) obtained from the theoretical analytical model (sub-chapter F.1);
- the maximum normal stress in the X-direction, 593,2 MPa, obtained with the finite element analysis (subchapter E.2.2) has a -1,13% deviation from the theoretical maximum normal stress (600 MPa) (subchapter F. 1);
- the shear stress distribution (E.2.3) highlights maximum values (14.26 MPa) in the compressed clamp

area having a deviation of - 4.9% from the theoretical value (15 MPa);

the equivalent stress (von Mises) has the maximum value (587.8 MPa) in the stretched clamp area.

G. CONCLUSIONS

On the first hand, the modelling and the finite element analysis from this application was done more with a teaching goal, in order to initiate the user with the main steps of developing an AEF application in ANSYS Workbench and, on the other hand, to compare and evaluate the results with some quasi-readings obtained through classical analytical models.

This process is recommended to be repeated for other practical situations in order to gain experience in developing analysis methods as well as evaluating the results.

The AEF model developed in this paper is inefficient from the point of view of the modelling possibilities offered by the ANSYS platform because it does not take into account the embedded connection area as well as the singularity associated with the concentric force due to the rough meshing with linear finite elements. These aspects are taken into account and studied in the application no. AEF-A.3.